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B. Zygmunt^{ab}; J. Visserª; U. A. Th. Brinkmanª; R. W. Frei^a

^a Department of Analytical Chemistry, Free University, Amsterdam, HV, The Netherlands ^b Technical

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Preconcentration and Analysis of Selected Pollutants in Industrial Effluents using LC Techniques

B. ZYGMUNT,t J. VISSER, **U. A.** Th. BRINKMAN **and** R. W. **FREI**

Depattment of Analytical Chemistry, Free University, De Boelelaan 1083, 1081 HV Amsterdam, The Netherlands

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The potential of using LC techniques for the analysis of industrial effluents has been explored. Twenty selected pollutants have been studied and investigated in standard solutions and actual waste water samples. The possibility of preconcentration and detection of most of these compounds at low levels $({\sim}1$ ppb) in effluent samples has been explored. LC techniques are not suitable for fingerprinting purpose. Their major strength lies in the isolation and determination of specific compounds, or groups of compounds, as demonstrated for the case of methyldiaminobenzene. An LC-grade styrene-divinylbenzene polymer, marketed by Hamilton (PRP,) has shown interesting characteristics to preconcentrate the majority of the pollutants studied. This approach coupled to chromatographic separation on the same materials and selective wavelength **UV** detection shows excellent potential for the analysis of priority pollutants in complex effluent samples.

KEY WORDS: Organic pollutants, XAD-type materials, preconcentration, water, samples, **UV** detection, HPLC, industrial effluents.

INTRODUCTION

It is well recognized that the determination of trace organic contaminants in water is fundamental to the solution of environmental protection problems. Since trace concentrations of organic pollutants are generally of interest, preconcentration prior to

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tOn leave of absence from the Technical University of Gdansk, Poland.

the analysis proper is often necessary. Beside extraction procedures, one of the most frequently employed methods of preconcentration of organic pollutants from water is direct extraction with solid sorbents.¹ Of all the sorbents, a low polarity styrene-divinylbenzene copolymer, Amberlite XAD-2, has been used most widely for the purpose.' Analytical procedures for the determination of organic pollutants in water employing Amberlite XAD-2 or chemically identical XAD-1 and XAD-4 presented in the literature include mainly off-line gas chromatographic techniques,¹ though a few online gas chromatographic (GC) methods have also been described.²⁻⁴ Procedures employing high-performance liquid chromatography (HPLC) are also very attractive and have a wider range of application than GC methods. Volpe and Mallet,⁵ e.g., employed offline HPLC techniques for the determination of fenitrothion and its seven derivatives in water. However, especially convenient should be on-line techniques. The advantages of on-line techniques have been pointed out in many papers⁶ and on-line HPLC techniques have become quite popular in the recent past. **Hux** *et aL7* used precolumns with Amberlite XAD-2 for direct injection HPLC determination of metaqualane in blood plasma while Cantwell and Mohammed⁸ used such precolumns for sample clean-up of complex pharmaceutical samples. However, as Werkhoven-Goewie *et* **aL9** mentioned, for HPLC analysis of a multi-component sample, a precolumn should be packed with HPLC-quality sorbents, i.e., having $5-10 \mu m$ particle diameter. Since Amberlite XAD-2 is usually supplied as the 20–50 mesh beads, a chromatographer is required to crush and resize the irregular particles.^{10,11}

Quite recently, a new spherical $10-\mu m$ styrene-divinylbenzene polymeric adsorbent, PRP,, has been introduced by Hamilton Company. Comparative study of PRP, and XAD-2 done by Lee and Kindsvater¹² has shown that the quantitative chromatographic characteristics of both sorbents are identical; PRP, having a higher surface area retains organic compounds even better than Amberlite XAD-2. Such retention characteristics and the fact that PRP_1 is in the form of spherical microparticles make Hamilton PRP, reversed-phase resin very suitable for on-line HPLC determination of trace organic pollutants in water. This paper describes the use of PRP_1 sorbent for on-line preconcentration and HPLC determination of aromatics with chloro and/or amino substituents in industrial wastewater.

Semiquantitative relationships between chromatographic retention and composition of the water/methanol mobile phase for the above mentioned compounds have also been established. They permit the prediction of breakthrough capacities (volumes) of precolumns and hence the attainable enrichment factors for a particular precolumn and pollutant at 100% recovery conditions. Breakthrough volumes of selected organic compounds on the **PRP,** precolumns predicted on the basis of the relationships derived have been compared with experimentally determined values.

TH EOR ETlCAL ASPECTS

The relationship between the capacity factor, *k',* and the volume fraction of organic modifier, ϕ , in reversed-phase HPLC on C_{18} bonded silica was studied by Schoenmakers *et al.*¹³ In general a non-linear relationship was found for aqueous systems containing $10-100\%$ of methanol which can be expressed as

$$
\ln k' = A\phi^2 + B\phi + C \tag{1}
$$

However, when using modifier in a ϕ range of at least 0.4–0.6 and with $k' > 1$ a linear approximation can be used for most solutes as follows:

 $\ln k' = \ln k'_{\text{H}_2\text{O}} - S\phi$

where *S* can be expressed as

$$
S = p + q \ln k'_{\text{H}_2\text{O}} \tag{3}
$$

 k'_{H_2O} is the capacity factor under pure aqueous conditions; *p* and *q* are empirically determined constants which depend on the stationary phase, type of modifier and column porosity.

 $\ln k'_{\text{H}_2O}$ can also be determined for many compounds of interest such as, for example, chlorophenols⁸ by measuring $\ln k'$ at two to three different ϕ values between 0 and 0.6 and then extrapolating the curve to $\phi = 0$. The retention volume, V_R , which permits computation of the trace enrichment factor, can be calculated from these extrapolated k'_{H_2O} values as

$$
V_R = V_0 (1 + k'_{H_2O})
$$
 (4)

 V_o , the dead volume, can be determined experimentally or calculated from the porosity factor, ε_0 , and the geometry (*r* = radius, *l* = length) of the precolumn as

$$
V_{\Omega} = \varepsilon_0 \pi r^2 l \tag{5}
$$

The relationship between V_R and the breakthrough volume, V_B , is given by **Eq. 6:**

$$
V_B = V_R - 2\sigma_v \tag{6}
$$

and σ_v (band broadening) can be determined from a breakthrough curve as described earlier.⁹

A typical schematic for on-line operation is shown in Figure 1. Pump **A** is used for sample loading or trace enrichment and pump B for the desorption and on-line transfer to the separation column. In order to keep band broadening at a minimum it is desirable⁶ that the same type of material (surface property and particle size) be used in precolumns and separation column. The length of the precolumn is usually very short (1-5mm) and the diameter equal or smaller **(4.6** to 1 mm I.D.) than that of the separation column.

FIGURE 1 Scheme of **on-line preconcentration procedure.**

EXPERIMENTAL

Reagents

The organic chemicals of interest and used to prepare standard solutions and spiked water samples are listed in Table I. The water used to study breakthrough curves and the analyses of artificial mixtures, and also for the mobile phase, was demineralized water filtered over a Millipore filter (Millipore, Bedford, MA, USA). Other solvents used were absolute methanol and acetonitrile, both Analysed Reagents from Baker (Deventer, The Netherlands) and methanol **p.a.** from Merck (Darmstadt, GFR).

The home-packed columns were packed with PRP, spherical chromatographic resin, manufactured by Hamilton Company (Reno, NE, USA). The PRP₁ analytical columns $(150 \times 4.1 \text{ mm})$ were manufactured by Hamilton Company and purchased from Kontron (Zurich, Switzerland). All other chemicals were of analytical grade.

'Source unknown

Chromatographic apparatus

A Spectra Physics 8000 (Santa Clara, CA, USA) liquid chromatograph was used for the measurements of the $\ln k'$ vs. ϕ curves and for a study of the influence of pH on *k'* values. It was programmed to give a constant flow of lml/min while the recorder was 10mV, and the UV detector range was set on 0.16AUFS $(\lambda = 254 \text{ nm})$.

The mobile phase solvents used with this apparatus were continuously degassed with helium to prevent the dissolving of air and the formation of air bubbles when mixing the two mobile phase components in the mixing chambers. At the end of the day the column was washed for about 20 minutes with pure methanol. For measuring the breakthrough curves a Kontron (Zürich, Switzerland) Analytical LC pump 410, a Kontron Uvikon 720 LC Spectrophotometer, a Kipp BD-8 multirange recorder (Emmen, The Netherlands) and a Rheodyne 990-3557 six-port valve (Berkeley, CA, USA) were used. The precolumn was a hand-packed 5×4.6 mm PRP₁ column.

For the separation of artificial mixtures and actual samples a Pye Unicam LC3 UV detector (Cambridge, England), a Kipp BD-8 multirange recorder, an Orlita TW 1515 double-head pump (Giessen, GFR) and a Rheodyne 089-0932 six-port valve were used. The flow was set to 1 ml/min and in all three setups the wavelength used was $\lambda = 254$ nm.

Analytical procedures

- *1. Sample preparation*
- -All stock solutions were prepared by weighing the compounds and dissolving in 10ml methanol. From these solutions, a milliliter or less was taken and diluted further with methanol if necessary, to make measurements concerning retention time, etc.
- $-$ For preconcentration and breakthrough measurements, 10–50 μ from the methanol solutions were taken and diluted in water up to 100-1000ml.
- Mixtures were made by dissolving several compounds in the same methanol solution, then diluted in water as above.

- For preconcentration of the real samples, the water was first filtered over a paper filter.
- $-$ To spike the real samples, a few μ of an artificial mixture were taken and added to the real sample solution.

2. Concentration on the precolumn Preconcentration of waste water and spiked waste water was carried out on a *5* mm x 4.6mm I.D. precolumn.

Different amounts of waste water were preconcentrated, and then on-line desorbed with methanol.

When using another mobile phase for desorption and separation, it was necessary to flush the precolumn with pure methanol after the desorption step and then briefly with water $(1-2m)$, before a new run was started.

3. Mobile phases The mobile phases used were water-methanol mixtures of different composition and prepared by premixing ultrasonicated solvents followed by degassing under stirring and vacuum. The bottle was then covered with parafilm to prevent the uptake of air.

For buffering the solutions to the various pH's, 0.1 M phosphate buffers were added so that the total buffer concentration in the solutions was 0.001 **M.**

RESULTS AND DISCUSSION

Measurement of In k' **vs.** ϕ **curves**

Several of the more polar compounds of our list (Table I), viz. the compounds B, *C,* F, **G,** L, **M,** 0, were investigated **as** to their retention at various ϕ values.

The above choice was made on the basis of preliminary experiments carried out on C-18 bonded silica with methanol as polarity modifier. These experiments showed that it was difficult to obtain a trace enrichment effect on C18-bonded silica supports since their retention was nil or very low and it was hoped to improve the situation on PRP, material. The curves, constructed from 4 to 8 data points, are shown in Figure 2. Since we are dealing with basic as well as acidic compounds, studies were carried out at three

FIGURE 2 Lnk' vs. ϕ curves, flow 1 ml/min, UV detection at 254 nm, curve 1-4 pH $= 3$, curve 5-8 pH = 7, curve 9, 10 pH = 8.3. Mobile phase: water-methanol, ϕ values **give methanol content; column lOOmm** x **4.6mm I.D. PRP, column. For identification** of compounds see Table I. Curve $(1) = M$, $(2) = C$, $(3) = G$, $(4) = F$, $(5) = O$, $(6) = L$, $(7) = D$, $(8) = B$, $(9) = Q$, $(10) = L$.

different pH's: *3,* 7 and **8.3.** Home-packed PRP, columns with between 500 and 700 plates (for the compounds examined) were used for these experiments.

From Figure 2 it can be seen that, as expected, nitrobenzene and p-chlorophenol are retained resaonably strong on PRP, at a pH of **3.** Retention for o-anisidine and dianisidine improved on going to pH 7 as shown in Figure 2 for the former. Very little retention has been found .at pH 7 for phenylenediamine and methyldiaminobenzene and going to pH **8.3** did not alter this situation. To buffer waste water samples to pH's much higher than this would hardly be feasible.

The influence of pH on the retention of some other compounds in Table I has been tested; the results are presented in Table 11. Chromatographic conditions were the same as in the previous study. From Table II the general trend is an increase in k' values in going from lower to higher pH and, as expected, also an increase in going to a lower methanol content. However, the differences with pH are small and as a result one can recommend, also in view of Figure 2, pre-concentration to be carried out at \sim pH 7.

From Figure 2 and some rough extrapolation work, one can also draw the preliminary conclusion that compounds with $\ln k'$ vs. ϕ

concentration						
Compound	$k'(\phi = 1.0)$	$k'(\phi = 0.9)$				
	pH 6.8	pH 2.7	pH 6.8			
в	0.7	1.3	1.4			
D	1.8	5.0	5.6			
Е	1.5	5.5	5.5			
F	--	--	1.1			
I	2.5	7.3	8.1			
J	3.0	10.7	11.75			
K	2.5	0.1	7.5			
M	1.6	3.7	3.7			
N	8.6		—			
	4.4		--			
Q S	2.8	6.7	6.8			

TABLE I1

k' **values for selected pollutants at different pH and methanol concentration**

plots to the right of curve 6 including all the other, even more retained compounds (Tables **I1** and **IV)** show a good preconcentration behaviour well above **10** ml sample volumes preconcentrated on a precolumn of 4.6mm **I.D.** and *5* mm length. **Of** the others the methyldiaminobenzene will probably show breakthrough at a sample volume < *5* ml and phenylenediamine even at < 1 ml (Table **111);** hence alternative preconcentration techniques would have to be thought for those if low ppb-values are required. **As** to the shape of the curves (Figure 2), one can also say that they are roughly linear, some perhaps tending slightly to a quadratic relationship, but at any rate linear extrapolation of such curves would provide a more conservative and hence safer figure and is recommended (see also later data on breakthrough curves; Table **111).** The only somewhat odd data points in Figure 2 were observed for phenylenediamine and methyldiaminobenzene at pH 8.3 for $\phi = 0.4$ and 0.45; for these, no explanation can be given.

Compound	Extrapolation		
	Quadratic curves V_R (ml)	Linear curves V_R (ml)	Experimentally found results V_R (ml)
B	477	14.7	14.4
C	606	17.4	24.5
F		43.3	45.5
L	3.6	1.6	3.0
	0.5	0.3	. а

TABLE 111

(Figure 2 and Eq. 4) Comparison of experimental V_R values with values calculated from extrapolation

'Too small to be **accurately determined by breakthrough curves.**

Breakthrough curves and retention volumes

From the above data it is possible to calculate breakthrough volumes and hence preconcentration factors without resorting to the tedious business of actually measuring breakthrough curves (see also theoretical introduction in this paper). This principle and the aspect and technique for determining breakthrough curves has been discussed in detail earlier for $C18⁹$ and for graphitized¹⁴ surfaces and recently for **PRP,** supports.15

A few breakthrough curves have also been measured in this study and compared to data obtained by quadratic and linear extrapolation to check the validity of our postulations. The results are presented in Table 111. One can observe a generallly good correlation between experimental data and the linear extrapolation approach. The precolumn used in these tests had a length of 2.5mm and 4.6mm I.D. The dead volume of the precolumn V_0 was determined according to Eq. 5 with ε_0 taken as 0.65 from the literature¹³ and was calculated to be \sim 27 μ l.

Separation of standard mixtures

The separation for a mixture of 15 compounds selected from Table I is shown in Figure **3.** Two compounds (N and Q) do definitely not show in the chromatogram since their retention on **PRP,** is too high under the prevalent mobile phase condition. Without attempting to identify the various peaks we can already say that for a good resolution of such a complex standard mixture a gradient would be necessary. It is also noticeable that strong tailing occurs, which is an inherent disadvantage of **PRP,** materials and results from poor mass transfer characteristics. An attempt was made to use a gradient from 70% to 100% methanol. Unfortunately the **PRP** material responded very sluggishly to changes in mobile phase composition and the pressure drop of the column increased by about 100 bar along with a rapid rise of the baseline. Such phenomena have been reported earlier for gradient work with **PRP** material and must be attributed to swelling of the polymer beads.

It was therefore decided to work with three different mobile phases (8: 1, 9: 1 and 1O:O methanol/water, pH 7) and to separate the compounds into **3** groups according to their suitability to be separated isocratically from the other members in the group. The three groups and the relevant *k'* values are shown in Table **IV.**

For the highly retained compounds one could also use **C18** in place of **PRP,** material since these can likely also be preconcentrated on **C** 18-bonded silica, with the advantage of being separable by gradient elution on the same material. Earlier work^{9,16} and some preliminary investigation in the course of this work

FIGURE *3* Separation of artificial mixture containing: B, C, D, **E,** F, **G,** I, **J, K,** L, M, N, O, Q and S. A 20μ l loop injection was done on a 100×4.6 mm I.D. 10μ m PRP₁ packed column; mobile phase, methanol-water (90:10), buffered with 0.01 M phosphate buffer to pH=7, at flow 1 ml/min; UV detection at 254nm, attenuation 0.08 **AUFS.**

Mobile phase:	$8:2 \text{ MeOH}:H_2\text{O}^*$	9:MeOH:H ₂ O	100% MeOH
Compounds	О	$B k' = 1.4$	$Mk' = 1.6$
	L	$E k' = 5.5$	$k' = 2.5$
	C	$K k' = 7.5$	$T k' = 3.4$
	F	$H k' = 6.6$	$k' = 2.8$
	G	$A k' = 8.8$	$Qk' = 4.4$
	D	$J \; k' = 11.7$	$R k' = 7.4$
		$P k' = 12$	$N k' = 8.6$

TABLE IV Mixtures suitable for isocratic separation for three different conditions

^{*}Order of appearance: $(k' 1-10)$: $O < L < C < F < G < D$.

~ ~ ~

support the feasibility of such an approach. Detection limits for the compounds tested were also determined at the chromatographic conditions suggested in Table **IV.** With absolute detection limits for most compounds being in the order of 1-20ng (using UV detection) and 10-ml sample volumes being feasible for most compounds for on-line preconcentration with short pre-columns, with 100% recovery it should be possible to detect these pollutants at about the lppb concentration range. The only borderline case of the compounds in Table I would be methyldiaminobenzene whereas phenylenediamine is hardly retained at **all.**

Analysis of real samples

Figure **4** shows a chromatogram for waste water taken after the biological cleaning step and preconcentrated on the usual precolumn

on a 5mm × 4.6mm I.D. column packed with $10 \mu m$ PRP₁ resin; sampling rate 5 ml/min. HPLC on 150 mm \times 4.6 mm I.D. column packed with 10 μ m PRP,; eluent **100%** methanol at 1 ml/min; UV detection at 220 nm, attenuation 0.04 AUFS.

and on-line transferred to the analysis column with a mobile phase containing 100% methanol. The detection wavelength was 220 nm. Chromatograms detected at **254** nm under otherwise identical conditions were even less conclusive. In general one can conclude that LC techniques are not very well suited for fingerprinting purposes and for a rapid assessment of the overall performance of a water treatment plant. The chromatographic resolution **is** much too low and GC techniques even with classical columns as described elsewhere 18 would have to be given preference.

However, LC techniques with on-line preconcentration show considerable promise for the isolation and detection of individual or small groups of pollutants as demonstrated with the following example. Figure 5 shows a chromatogram for a 4-ml waste water

FIGURE 5 Identification of compounds in a waste water sample. 4ml sample preconcentrated. All conditions as in Figure 4 except for HPLC eluent (9: 1 methanolwater buffered to $pH = 7$ with 0.01 M phosphate buffer) and attenuation (0.4 AUFS). **Figure 5a waste water. Figure 5b p-chlorophenol, 10** μ **l injection (0.1 mg/ml). Figure 5c** 1-methyl-2, 4-diaminobenzene, $10 \mu l$ injection (0.25 mg/ml) .

sample preconcentrated in the usual manner and separated with a 9:1 (v/v) methanol/water mixture on a PRP_1 column. The detection wavelength is again 220nm. According to *k'* values peaks *b* and c can be assigned to p-chlorophenol and methyldiaminobenzene respectively. Further evidence for the presence of the latter compound was gathered. Detection at different wavelengths was also investigated as shown in Figure **6** were chromatograms for 4ml samples are recorded at 200, 220, 254 and 280nm, respectively using a variable wavelength UV detector. Good evidence for the actual presence of methyldiaminobenzene can be gathered from these chromatograms when comparing them to standard chromatograms of the pure compound detected at the same wavelength. Very clear and reasonably well separated peaks can be observed for 200 and 220nm detection, whereas with 254 and 280nm the compound is barely visible which is in accordance with the **UV** absorption spectrum for this compound.

FIGURE *6* Analyses of 4ml preconcentrated water samples at four different wavelengths. All conditions as in Figure 4 except for HPLC eluent (9:1 methanolwater) **UV** detection at (a) 220nm attenuation 0.4AUFS, (b) 254nm attenuation 0.4 AUFS, (c) nm attenuation 0.4 **AUFS,** (d) 280 nm attenuation 0.2 AUFS. Arrow points to the peak of interest **(l-Methyl-2,4-diaminobenzene).**

Although the quantitation aspect of this technique has not been further explored, there is good evidence that standard addition techniques can be used to quantitate certain compounds, provided that they are reasonably well separated. The enhanced selectivity obtained through proper selection of detection wavelength in UV detection is quite promising.

CONCLUSIONS

On-line pre-concentration of the 20 pollutants investigated (Table I) is essentially possible on **PRP,** sorbents with the exception of phenylenediamine (< 1 ml). For methyldiaminobenzene only below 5ml sample sizes are possible. With on-line transfer of the enriched sample to the separation column no further losses or contamination can occur and the method can be fully automated if required. It should be realized that even with 10ml samples an enrichment factor of 100 is obtained by this pre-concentration technique.

The use of C_{18} sorbents for the less polar compounds can be complementary to **PRP,** sorbents with the advantage of being compatible with gradient elution techniques. This is not the case for **PRP,** sorbents where swelling of the beads prevents the use of gradient elution; hence compounds have to be classified in groups for isocratic separation. The suitability of **HPLC** techniques for fingerprinting purpose is rather doubtful. The major strength of the **HPLC** approach lies in the possibility to selectively determine specific pollutants. This has been demonstrated with the detection of methyldiaminobenzene in effluent water using selective wavelength detection. Obviously definite proofs would have to be given by **MS** as an on-line or off-line detection device.

Nevertheless this points in the direction of use of diode array UV detectors, such as now commercially available from various companies, for isolation of single compounds or groups of compounds (selective mapping) in complex sample matrices. The use of other possibly more selective sorbents (other than PRP_1 and C_{18}) such as ion exchangers and metal-loaded supports for selective preconcentration of ionic and (or) complexing pollutants is currently investigated and shows good promise (i.e. pre-concentration of chlorophenols on anion exchanger). Another approach with good possibilities is the coupling of pre-column technology with selective detectors (see also refs. 14, 6). **A** recent example was the selective detection of chlorophenols by photolytic dechlorination and fluorescence detection of the non-substituted phenol produced.¹⁴ Reaction detectors such as this show particularly interesting possibilities.¹⁷

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Appendix

COLUMNS AND COLUMN PACKING PROCEDURE

Several PRP₁ columns were used: home packed 15 cm $(N = 865)$ and 10 cm $(N = 1290) \times 0.4$ cm I.D. columns, and Hamilton 15 cm \times 0.4 cm

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I.D. columns $(N = 1120)$. A packing procedure slightly modified from the one described by Lee and Kindsvater¹² was used. The columns were packed as follows: The resin (1 g) was slightly moistened with acetone and then some packing solvent was added. When the slurry was good, more packing solvent was added up to a total of 20ml slurry. The packing solvent was 2.5% sodium chloride and 20% glycerine in water. The slurry was agitated under vacuum in an ultrasonic bath and the column was filled with the slurry. Then the tube was connected to the slurry vessel filled with the rest of the slurry and then with packing solvent. The tube was connected to a Haskel pneumatic pump and the column was packed downward at 5000 psi. After 3 strokes $(\pm 30 \text{ min})$ the column was disconnected from the tube. The plate number of the columns were tested using a 9: 1 MeOH: H,O mobile phase and nitrobenzene as a test compound. With this mobile phase nitrobenzene has a *k'* value of 3.5 which is sufficiently high to give a reliable value of the plate number.